Eddy Currents and Magnetic Calibrations in LDX using a "Copper Plasma"

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"Copper Plasma" Overview

- LDX Magnetics
- Goals
 - Calibrate magnetic diagnostics positions and gains
 - Find eddy current decay times
- Copper Plasma Operation
- Theory
- Analysis
- Results

LDX Magnetics

18 external magnetic field sensors

- 9 parallel
- 9 normal
- *n* ≈ 1000 turns, *a* ≈ 50 cm², 15 cm length
- 9 external flux loops
- 5 internal flux loops
- Sensors are time integrated using RC circuits



VPPER CATCHER WITH INTERAL FLVX LOOPS









$$\vec{A}(r, z, R, Z, I) = \mu_0 IR \frac{(2 - k^2)K(k^2) - 2E(k^2)}{\pi k^2 \sqrt{(r + R)^2 + (z - Z)^2}} \hat{\varphi}$$

$$k^{2} \equiv \frac{4rR}{(r+R)^{2} + (z-Z)^{2}}$$

$$B_{z} = \frac{1}{r}\frac{\partial}{\partial r}rA_{\varphi} ; B_{r} = -\frac{\partial}{\partial z}A_{\varphi}$$

$$\Phi = \int \vec{B} \cdot d\vec{a} = \oint \vec{A} \cdot d\vec{\ell} = 2\pi rA$$

$$\Phi = \int \vec{B} \cdot d\vec{a} \approx \vec{B} \cdot n\vec{a} = na(B_{z}\cos\theta + B_{r}\sin\theta)$$

$$V = \frac{1}{RC}\int -\frac{d\Phi}{dt}dt = -\frac{\Phi}{RC}$$

Goal: Calibrate Magnetics

- Positions of sensors *r, z, θ* have been measured with rulers and laser level
 Accuracy ~ 3mm / 1°
- Gains *g* of integrator boards have been measured electronically
- Would be better to measure positions and total gains <u>magnetically</u>

Goal: Eddy Currents

Magnetic levitation vertically unstable

- Requires active feedback control
- Fluctuations in L-coil, F-coil and plasma current magnitude
- Fluctuations in F-coil and plasma position

Changing currents induce eddy currents in vessel

- Eddy currents are picked up by magnetic diagnostics
- Must be measured so they can be properly included in magnetic reconstruction
- L- and F-coil eddy currents measured in vacuum shots
 - L-coil only shots know position, know current
 - Use L-coil to induce vertical jog in F-coil, measure position with lasers and calculate current from force balance

How to estimate eddy currents due to fluctuating plasma currents?

Changes in plasma current magnitude and position **NOT** known

Solution: Build "Copper Plasmas"

- 2 coils of 12 AWG copper wire
 - Approximately same radius as plasma
 - □ **R** = 76 cm coil 28 turns, 91 cm coil 25 turns
 - Built on plywood forms, forms disassembled and reassembled in vessel, coils squeezed through port
- Operated in 3 vertical positions
 - From midplane, $\boldsymbol{Z} = 0, \pm 5 \text{ cm}$
- L-coil control system used to impose trapezoidal current pulses
 - 4s flattop @ 60A
 - Rise and fall times: 0.5s, 1s, 2s
- Operated with + and polarity by switching coil leads
- 2 R x 3 Z x 3 times x 2 polarities x 31 sensors

Photo of copper plasma



Theory: Calibrate Magnetics

- By using copper plasma with 2 different radii *R* at 3 different heights *Z*, can use least squares fit to find sensor calibration
 - 6 equations to find 3 or 4 unknowns
- Copper plasma parameters also not known exactly, can use least squares to find them
 - 2 R x 3 Z x 31 sensors = 186 equations to find 15 unknowns
- V(x_c, x_s) is non-linear
 - Linearize using measured parameters
 - Solve linear least squares
 - Adjust parameters and repeat
 - Switch between solving for *x_c* and *x_s*



Results: Calibrate Magnetics

- Flux loops give reasonable results
 - Calculated locations mostly within ~2 cm of measured
 - Gains mostly within ~10% of measured
 - \mathbf{X}^2 goodness of fit ~ 10⁻³
 - Copper plasma location also found within 1 cm of measured
- Magnetic sensors have very large errors
 - \mathbf{X}^2 goodness of fit too small for floating point
 - Because of poor results, not used in solving for copper plasma location

Theory: Eddy Currents

- Measured voltage V given by sum of all coil and eddy currents I times their respective Green's functions G
- In reality, many eddy current modes occur
- To simplify, assume one dominant mode per sensor
- Final equation requires no knowledge of eddy currents to calculate decay time, $\tau_{\rm E}$

(1)
$$V_{j} = G_{c,j}I_{c} + \sum_{E}G_{E,j}I_{E}$$
 (2) $\tau_{E}\frac{dI_{E}}{dt} + I_{E} = k_{cE}\tau_{E}\frac{dI_{c}}{dt}$
(3) $V_{j} - G_{c,j}I_{c} = -\tau_{E,j}(\frac{dV_{j}}{dt} - (G_{c,j} - G_{E,j}k_{cE,j})\frac{dI_{c}}{dt})$

Analysis: Eddy Currents

- Using the *I* and *V* waveforms from each of the 31 sensors and 36 experiments :
 - Steady state Green's function G_{c,j} is ratio of flattops
 VO / IO
 - This is the quantity used in sensor calibration
 - *d/dt* dominated Green's function *G_{c,j} k_{cE,j}G_{E,j}* is ratio of slopes *dV/dt / dI/dt* at some initial time
 - τ_{E} found by least squares fit to Eq. 3





Uncertainty Analysis

Most uncertainty due to integrator drift

- Circuits have some drift compensation
- In analysis, subtract initial drift before pulse
- Optionally subtract drift during flattop and after pulse
- Find average drift and uncertainty as a function of time from shots with no current
- Sum shots with opposite polarity to cancel out stray fields and any reproducible drifts
- Also some uncertainty due to power supply
 - Current is somewhat noisy
 - Difficult to fit initial *d/dt* on small, noisy signal
 - Feedback system designed for L-coil, not copper plasma
 - Leads to ringing at corners of trapezoid



Results: Eddy Currents

- Most sensors in range 30 70 ms
 - Standard deviations over all shots 3 5 ms
 - Consistent with predictions from theory
- Some < 10 ms or negative, standard deviations as big as τ_E





- Sensor calibration and eddy current decay time results generally consistent with previous measurements
- Copper plasma experiment did not yield an improvement in accuracy or precision over previous measurements

Suggestions for Future Work

- Work to reduce integrator drift
- Optimizing power supply for copper plasma could reduce noise and ringing
- Use less simplified model for copper plasma and sensors
 - Multiple windings in copper plasma
 - Possible errors in construction
 - Area and length in magnetic sensors
- Try more robust fitting schemes for calibration
- Improve calculation of k_{cE,j}G_{E,j}
 - Use different pulse shape faster rise time, sinsusoid
 - Use non-linear method to solve for both τ_{E} and $k_{cE,i}G_{E,i}$
- Do more complete analysis with multiple eddy current modes

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