

Levitation Control System for the Levitated Dipole Experiment

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Abstract

- The confining field in the Levitated Dipole Experiment (LDX) is provided by a 1/2 ton levitated superconducting dipole magnet. This floating coil is charged with 1.5 MA current and will be levitated continuously for the eight hour experimental run day.
- Earnshaw's theorem states that there exists no statically stable configuration for levitation of magnets. In LDX, the floating coil is levitated by a smaller dipole levitation coil 1.5 meters above. This configuration is unstable vertically, but stable in tilt or horizontal motion.
- The position of the coil will be monitored with a set of eight laser position detectors giving redundant measurements of the five degrees of freedom of the floating coil.
- The levitation will then be stabilized by feedback control of the current in the levitation coil. The feedback system is a digital system running on a real time operating system platform. This system is programmed, monitored, and controlled by a second computer using Matlab Simulink. The system is currently being tested on a small model and a larger test is planned before LDX operation.
- Results from these tests and optimizations are presented.

Outline

- Introduction to LDX
- Coil Systems
 - ≻ F-coil
 - L-coil
 - TSR coils
- Levitation Physics
- Levitation Control System
 - Hardware
 - Optical detection system
 - Digital real-time control computer
 - Simulation
 - Cheerio Model
- Conclusions

LDX: Experimental Overview

- LDX consists 3 major components:
 - a high performance super conducting floating coil
 - charging coil
 - vacuum vessel
- Other components include
 - Plasma heating system (multifrequency ECRH)
 - Levitation coil
 - Control system & coils
 - Launcher/Catcher system
 - Plasma shaping (Helmholtz) coils
 - Plasma diagnostic systems



Charging (C) Coil and Cryostat

5 m dia Vacuum Vessel

LDX Experiment Cross-Section



Levitation Control System Schematic



High T_c Superconducting Levitation Coil

- SBIR collaboration with American Superconductor to build first HTS coil in the fusion community.
- Uses 7kmof BSSCO-2223 conductor
 - > 1128 turns 1-in-hand wound
 - > 37 Joints
- Max field 0.8 Tesla
- 20 kJ stored energy can be dumped in < 1 second.
- Cryostat is cooled with cryocooler 30W cooling capacity at 20° K
- Feedback gain selected for 5 Hz frequency response
 - Limit heating to < 20W AC losses</p>
- Manufacturing underway at Everson
 Electric



LDX Floating Coil

- Unique high-performance Nb3Sn superconducting coil
 - 1.5 MA-turns, 800 kJ
 - 580 kg weight
 - 8 hr levitation
- Successfully tested
 - July 2000: Tested on-site at MIT above design current
- Cryostat under construction





F-Coil Cross-Section



- 1. Magnet Winding Pack
- 2. Heat Exchanger tubing
- 3. Winding pack centering clamp
- 4. He Pressure Vessel (Inconel 625)
- 5. Thermal Shield (Lead/glass composite)
- 6. Shield supports (Pyrex)
- 7. He Vessel Vertical Supports/Bumpers
- 8. He Vessel Horizontal Bumpers
- 9. Vacuum Vessel (SST)
- 10. Multi-Layer Insulation
- 11. Utility lifting fixture
- 12. Laser measurement surfaces
- 13. "Visor" limiter attachment

Optical Position Detection System

Position/Attitude Sensing

- Occulting system of 8 beams
- Provides measurement of 5 degrees of freedom of coil with redundancy in each measurement
- Specification
 - ± 1 cm detection range
 - 5 µm resolution
 - 5 kHz frequency response
- Current Status
 - Tests of 1st channel of optical system performed August 2001
- Rotation Sensing
 - Reflecting system to sense final degree of freedom
 - Nonaxisymmetry systematic noise correction



Digital Control System Schematic



- Design Requirements
 - All digital process control
 - Mathworks Matlab/Simulink design tool and visualization software
 - Process control on hard real-time operating system based computer
- Modular QNX Neutrino based system Real-time system
 - Opal-RT RT-Lab interface to Simulink with hardware drivers
 - Multiple I/O boards
 - 32 Analog Inputs
 - 16 Analog Outputs
 - 64 Digital I/0 channels
 - 50 kHz maximum hardware synchronized loop update rate
 - System is upgradable in both number of channels and processing power

Levitation Physics

We can choose a Lagrangian formulation of the equation of motion so the constraints above can be easily incorporated:

$$L = \frac{1}{2} \sum_{i=1}^{6} m_i \mathcal{K}_i^2 - M_{LF} I_F I_L - \frac{1}{2} L_F I_F^2 - \frac{1}{2} L_L I_L^2 - mgz$$



Where: $M_{LF} = M_{LF}(\vec{x}_{1\rightarrow 5})$

F-coil is a superconducting loop, so its flux is conserved, whereas we can vary the flux in the L-coil by applying our control voltage:

$$\Phi_F = M_{LF}I_FI_L + L_FI_F = \text{constant}$$

And:

$$\Phi_L = M_{LF}I_FI_L + L_LI_L = \int V_L(t)dt$$

Levitation Physics - Simulink Model

... solving for the magnetic force on the F-coil due to the L-coil in terms of the flux gives:

$$F_{magnetic} = \vec{\nabla} M_{LF} \frac{(M_{LF} \Phi_F - L_F \Phi_L)(M_{LF} \Phi_L - L_L \Phi_F)}{(L_L L_F - M_{LF}^2)^2}$$

This equation translated to a Simulink model might look like:



Feedback stabilization

- The upward force on the F-coil is proportional to the radial magnetic field at its position, generated by the L-coil.
 - > Hence, it is proportional to the current in the L-coil.
- Without feedback, the vertical position is unstable because dBR/dz>0, so if the F-coil moves up, the upward electromagnetic force will increase, and the coil will move even further up.
- If we detect a small increase in vertical position, and decrease the L-coil current appropriately, we can bring the coil back to its original position.
- Simple Approach: Use proportional-integral-derivative (PID) feedback:

$$I_L(t) = I_0 - a_0 \int \varepsilon(t) dt - a_1 \varepsilon(t) - a_2 \varepsilon \mathfrak{C} t$$

Automatic correction to I_0

Damping term, acts like friction

Feedback: Optimized Voltage PID

 Because of the L-coil inductance, we cannot change IL instantaneously. We can control the voltage=L*dIL/dt, instantaneously (or as fast as the power supply allows us to change its voltage):

$$V_L(t) = -b_0 \varepsilon(t) - b_1 \varepsilon (t) - b_2 \varepsilon (t)$$

• Include an integral term to automatically adjust for DC losses:

$$V_L(t) = -b_{-1} \int \varepsilon(t) dt - b_0 \varepsilon(t) - b_1 \varepsilon (t) - b_2 \varepsilon (t)$$

- The b parameters are optimized to get the best stabilization:
 - Put feedback expression into equation of motion to find most stable, critically damped solution
- Technique used to estimate required currents / voltages for L-coil
- Similar technique (using only derivative gain) used to determine required current for damping Rock & Roll motion using TSR coils
 - ~ 200 Amp turns required...

L-coil Heating

- Heating at 20K dominated by AC losses⁽¹⁾
 - ➢ F-coil vertical oscillation of 1 mm at 1 Hz ⇒ ±1 A 1 Hz oscillation in L-coil current ⇒ 20 W heating
- Suppress feedback gains at high frequencies to limit AC losses
 - > Derivative terms in feedback are particularly noise sensitive
 - > Very high frequencies (1/ ω < 15 msec) are shielded by vessel
- Current design for L-coil has cryocooler with 30 W capacity at 20 K
 - Finite element analysis ⁽²⁾ shows that internal temperature differences can be kept below 10 K if heating power is less than 100 W



⁽¹⁾ J. H. Schultz et al., presented at ASC conference, September 2000
 ⁽²⁾ R. L. Myatt, Myatt Consulting, Inc.

LCX II: Digitally Controlled Levitation





- Levitated Cheerio Experiment II
- Uses LDX digital control system
 - LCX I was analog demonstration
- Modified PID feedback system
 - Low pass filter added for high frequency roll-off of derivative gain
 - Integral reset feature for launch transition
- Dynamic model block replaced by I/O and estimators
- Real-time graph shows position and control voltage
 - Wiggles indicate non-linearly stable rolling mode...

Basic Simulink Levitation Model



• This basic model simulates 6 degrees of freedom of F-coil with L-coil levitation using voltage feedback control.

Basic Levitation Model Results



- Control parameters as calculated from analytic optimization for voltage PID loop
 - Simulations stay within L-coil supply specifications
- Simulink works!
 - Results match previous numercal simulations
 - Analytic analysis eigenmodes are 1.0 and 0.4 Hz
 - Single afternoon of work
- On to implementation!

System Simulink/Stateflow Model



L-coil Power Supply Simulation



- Model of 12 pulse power supply for L-coil
 - Uses Simulink Power System Blockset
 - > Will upgrade to use Opal-RT Artemis for extensive simulation
- Internal voltage control feedback loop
 - > Possible to use phase control directly in our completed system

Stateflow diagram of Control System



State System Simulation



- Complete functional model
 - Includes human check wait states
 - Automatic failure modes tested
- Z Position Graph
 - Shows launcher in action
 - Current ramp of L-coil
 - Pre-flight check
 - (Premature) launch
 - Free flight

More Full Simulation Results







- Vibrating launcher spring
- L-coil supply voltage ripple
 - ~ 40 volt ripple
 - Current ripple is < 50mA</p>
 - No filtering required
- Some state machine bugs...

Future Development





- Optimal Control Theory
 - Use Matlab control system toolbox
 - Characterize system
 - Develop optimal feedback control algorithm
- Hardware Integration
- Testing program
 - Use light small aspect ratio magnet
 - optical system calibration
 - Integrated supply test
- Further algorithmic / state machine testing

Conclusions

- Levitation Control System Design Complete
- Control coils designed, specified, and being purchased
 - > Modern HTS L-coil... first in Fusion research!
 - Modest power supply requirements specified
 - TSR coil size specified (and very modest)
- Digital Control System Under Development
 - Computer hardware / software in place
 - Several demonstrations / simulations made to show feasibility
- Hardware implementation being designed and tested
 - > 1st channel of optical system under evaluation
- Control algorithms under development